

## Effects of water and fluorine on the viscosity of albite melt at high pressure: a preliminary investigation

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The viscosities of fluorine- and water-bearing melts based on albite composition have been determined at 7.5, 15 and 22.5 kbar by the falling-sphere method. All melt viscosities decrease isothermally with increasing pressure. At 1200°C the viscosity of the fluorine-bearing melt (albite + 5.8 wt.% fluorine substituted for oxygen, denoted AbF<sub>2</sub>O<sub>1</sub>) decreases from 5000 ± 750 P at 7.5 kbar to 1600 ± 240 P at 22.5 kbar. At 1400°C the viscosity of this melt decreases from 1300 ± 200 P at 7.5 kbar to 430 ± 65 P at 22.5 kbar. At 1400°C the viscosity of albite + 2.79 wt.% water (denoted AbH<sub>2</sub>O) decreases from 650 ± 100 P at 7.5 kbar to 400 ± 60 P at 22.5 kbar. Fluorine (as F<sub>2</sub>O<sub>1</sub>) and water strongly decrease the viscosity of albite melt over the entire range of investigated pressures. The ratio of the effects of 5.8 wt.% fluorine [F/(F + O) molar = 0.10] and 2.79 wt.% water [OH/(OH + O) molar = 0.10] on the log of melt viscosity [ $\Delta \log \eta(\text{AbF}_2\text{O}_1)/\Delta \log \eta(\text{AbH}_2\text{O})$ ] equals 0.90 ± 0.05, 0.84 ± 0.05 and 0.97 ± 0.05 at 7.5, 15 and 22.5 kbar, respectively.

Comparison with available data on the high-pressure viscosity of albite melt indicates that both F<sub>2</sub>O<sub>1</sub> and H<sub>2</sub>O maintain their viscosity-reducing roles to lower crustal pressures. The difference between the viscosities of melts of albite, AbF<sub>2</sub>O<sub>1</sub> and AbH<sub>2</sub>O, may be explained in terms of the relatively depolymerized structures of AbF<sub>2</sub>O<sub>1</sub> and AbH<sub>2</sub>O melts. The depolymerization of albite melt by the addition of water results from the formation of Si–OH bonds. The depolymerization of albite melt by F<sub>2</sub>O<sub>1</sub> substitution results from the formation of non-bridging oxygens associated with network-modifying aluminum cations that are formed upon fluorine solution.

The strong viscosity-reducing effects of water and fluorine in albite melt at pressures corresponding to the mid- to lower continental crust indicate that these two components will strongly influence the dynamic behavior of anatectic melts during initial magma coalescence and restite-melt segregation.

### 1. Introduction

Viscosity is a fundamental property that influences the dynamic behavior of silicate melts [1–3], and dynamic processes such as melt segregation, magma mixing, crystal fractionation and fluid exsolution contribute to the compositional diversity of igneous rocks observed at the earth's surface. In addition, owing to the large compositional dependence of viscosity in silicate-melt systems, this property has been used as a tool for the investigation of melt structure in certain systems [4,5].

The pressure dependence of the viscosity of various silicate melts varies strongly with chemical composition [6–8]. Depolymerized melts such as those of diopside and sodium metasilicate composition experience a viscosity increase with in-

creasing pressure [6], whereas more polymerized melts such as those of albite and jadeite composition show a decrease in viscosity with increasing pressure [7,8]. The magnitude of pressure dependence also depends on melt composition, although the data available are insufficient for generalization of the pressure dependence of silicate melts.

Two chemical components that drastically alter silicate-melt viscosities are fluorine and water [9,10]. The pressure dependence of the viscosities of water-bearing melts has received some attention [10,11], whereas the pressure dependence of the viscosities of fluorine-bearing melts has not been investigated. The viscosities of water- and fluorine-bearing melts are useful for a direct comparison of the relative depolymerizing effects of these components. With this in mind, the high-

pressure viscosities of two melts, one fluorine-bearing and one water-bearing, have been investigated. Albite was chosen as the base composition for this study because its high-pressure viscosity is known [7], the structure and properties of albite melt have been studied by several workers [4,12-14] and albite is an important component of many fluorine- and water-rich igneous rocks.

## 2. Experimental methods

The viscosities of the melts were determined with the falling-sphere method. Starting materials for the viscometry experiments were water-bearing (2.79 wt.% H<sub>2</sub>O) and fluorine-bearing (5.8 wt.% F) glasses. Anhydrous albite glass was made from reagent-grade Na<sub>2</sub>CO<sub>3</sub>, Al<sub>2</sub>O<sub>3</sub> and SiO<sub>2</sub>. A mixture of oxides and carbonate was decarbonated at 400°C and fused at 1400°C. Small, known amounts of water were added to 200-250 mg of powdered albite glass, sealed in platinum capsules and fused in a solid-media, high-pressure apparatus at 1400°C for 1 hour. The resulting, water-under-saturated, albite glass was bubble-free and was used in the high-pressure viscosity measurements. The synthesis and analysis of the fluorine-bearing glass have been described previously [9]. The fluorine was added to the base composition by substituting 2AlF<sub>3</sub> for some of the Al<sub>2</sub>O<sub>3</sub>. Thus the substitution is 2 moles of fluorine for one mole of oxygen, denoted by the exchange operator, F<sub>2</sub>O<sub>-1</sub> (molar). The quantities of fluorine and water incorporated in the melt used in this study are equivalent in terms of the molar quantity  $X/(X+O)$  where  $X = F, OH$ . The substitutions are described by the following equations:



In this study  $x = 0.418$ . This value corresponds to  $X/(X+O) = 0.10$ . In the following discussion the water- and fluorine-bearing melts are referred to as AbH<sub>2</sub>O and AbF<sub>2</sub>O<sub>-1</sub>, respectively. These compositions are plotted in the system NaAlSi<sub>3</sub>O<sub>8</sub>-F<sub>2</sub>O<sub>-1</sub>-H<sub>2</sub>O in Fig. 1. Electron microprobe analyses of the albite and AbF<sub>2</sub>O<sub>-1</sub> glasses are presented in Table 1.

Platinum capsules for viscometry runs (10 mm

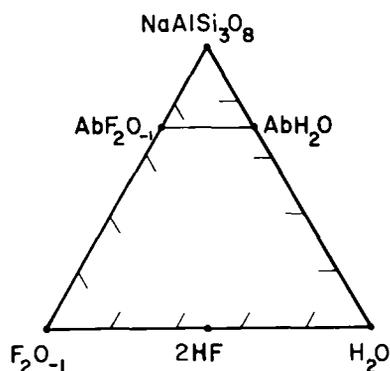


Fig. 1. Melt compositions AbH<sub>2</sub>O and AbF<sub>2</sub>O<sub>-1</sub> in the system NaAlSi<sub>3</sub>O<sub>8</sub>-H<sub>2</sub>O-F<sub>2</sub>O<sub>-1</sub> (in mole percent).

long, 5 mm diameter) were tightly packed with powdered AbH<sub>2</sub>O or AbF<sub>2</sub>O<sub>-1</sub> glass, and spheres of platinum and rhodium were placed on the top of the charge. A very small amount of fine (less than 1 μm) platinum powder was placed at this level to mark the starting position of the spheres, and a thin layer of powdered glass was packed above the spheres to prevent them from sticking to the capsule.

The viscometry experiments were conducted in a solid-media high-pressure apparatus by methods described previously [8,15]. Sealed platinum capsules were placed within 3/4"-diameter furnace assemblies with tapered graphite heaters to reduce temperature gradients [8]. The temperatures were measured with a Pt-Pt10Rh thermocouple with no correction for the effect of pressure on electromo-

TABLE 1

Starting compositions

Element <sup>a</sup>	Albite	AbF <sub>2</sub> O <sub>-1</sub>	Stoichiometric albite
Na	8.79	8.31	8.74
Al	10.36	9.15	10.29
Si	31.95	31.54	32.12
O	48.76	44.5	48.84
F	-	5.8	-
Total	99.86	99.30	100.00

<sup>a</sup> Na, Al and Si determined by electron microprobe; O determined by stoichiometry; F determined by neutron activation analysis. (F is ±0.1 wt.% at 1σ.)

tive force. The experimental runs were raised to final run pressure plus 15–20% (except at 7.5 kbar where the runs were overpressured to 15 kbar during initial heating) and then heated to 400°C below run temperature and held there for 1 minute while the pressure was trimmed to run pressure. The pressure correction for this procedure is –3%, as calibrated with the quartz-coesite transition. Finally, a rapid approach to run temperature was achieved (400°C/min) with an automatic controller.

A time series of three experiments was performed for each viscosity determination. The experiments ranged in duration from 4 to 200 minutes and were quenched by turning off power to the heater. This procedure resulted in quench rates of greater than 250°C/s. After an experiment, the run capsule was sawed lengthwise on two opposite sides to remove part of the platinum-capsule walls. The resulting flat plate of glass was taped to the X-ray film holder of a flat-plate camera, and the film was exposed to Mo white radiation (35 kV, 12 mA) for 10 seconds [15]. The sphere positions were measured from the developed film with a microscope.

### 3. Results

Graphs of time vs. distance were constructed for each sphere size, and straight lines were fitted to the data (Fig. 2). These time-distance lines pass through the origin, within error. Although melt densities can be calculated from the data obtained in this study, analysis of errors resulting from propagation of the errors in sphere radii and velocities yields large density uncertainties because of the large density contrast between the melts (2.5–3.0 g/cm<sup>3</sup>) and the metal spheres (12–21 g/cm<sup>3</sup>). In this study the densities of quench glasses, determined by the method of Berman [16], were used in the calculation of melt viscosities. The melt densities are probably 10–20% lower than the measured glass densities [8]; owing to the large density contrasts between the melt and metal spheres, however, the effect on calculated melt viscosities is insignificant. Sphere velocities, sphere radii and glass densities were used as input data for a FORTRAN program that incorporates cor-

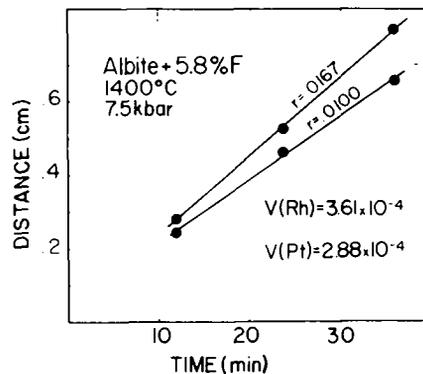


Fig. 2. Relation between time and distance of sinking of metal spheres (radii,  $\pm 0.01$  cm; velocities,  $\pm 5\%$ ).

rections for metal compressibilities and thermal expansivities [17] and the Faxen correction [10] for wall effects and solves for melt viscosity. Propagation of the uncertainties in sphere position and size yields estimates of  $\pm 15\%$  for viscosity.

The glass densities, sphere sizes and sphere velocities are presented in Table 2 together with the computed melt viscosities. In Fig. 3 the data from this study are compared with data for albite melt (1400°C) and 0.001 to 20 kbar [4,7], for  $\text{AbF}_2\text{O}_1$  melt (1200–1400°C and 0.001 kbar, [9]) and for low-pressure (1–2 kbar)  $\text{AbH}_2\text{O}$  melt calculated by the method of Shaw (1400°C, [18]).

The viscosity of the  $\text{AbF}_2\text{O}_1$  melt decreases

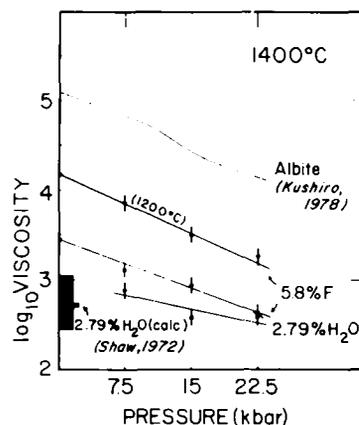


Fig. 3. Experimental results and comparison with data for albite melt [4,7]; fluorine-bearing albite melt at 1 atm [9] and water-bearing albite melt (calculated [18]).

TABLE 2

Experimental conditions and results <sup>a</sup>

Composition	<i>T</i> (°C)	<i>P</i> (kbar)	Radius (× 10 <sup>-2</sup> cm)	Speed (× 10 <sup>-4</sup> cm/s)	$\rho_{\text{glass}}$ (g/cm <sup>3</sup> )	Viscosity (P)	
						mean	
AbH <sub>2</sub> O	1400	7.5	1.33Rh	5.20	2.33	611	650
			1.00Pt	5.22		679	
		15.0	1.33Rh	8.00	2.33	397	370
			0.87Pt	6.80		337	
		22.5	1.33Rh	7.50	2.38	424	400
			1.00Pt	9.52		374	
AbF <sub>2</sub> O <sub>-1</sub>	1400	7.5	1.67Rh	3.61	2.36	1324	1300
			1.00Pt	2.88		1229	
		15.0	1.67Rh	5.35	2.39	895	820
			1.00Pt	4.72		751	
		22.5	1.67Rh	9.57	2.41	459	430
			1.00Pt	9.83		400	
	1200	7.5	1.03Pt	0.68	2.42	5486	5000
			1.70Pt	2.07		4534	
		15.0	1.25Pt	1.96	2.46	2748	2900
			1.00Pt	1.20		2964	
		22.5	1.50Pt	4.67	2.48	1612	1600
			1.03Pt	2.47		1524	

<sup>a</sup> Uncertainties are as follows: *T*, ±10°C; *P*, ±0.5 kbar; radius, ±0.001 cm; speed, ±5%;  $\rho_{\text{glass}}$ , ±0.01 g/cm<sup>3</sup>; viscosity, ±15%.

with increasing pressure from 0.001 to 22.5 kbar. The decrease in viscosity is similar at 1200°C (17,800 ± 900 P at 0.001 kbar to 1600 ± 240 P at 22.5 kbar) and at 1400°C (2900 ± 150 P at 0.001 kbar to 430 ± 65 P at 22.5 kbar). The pressure dependence of viscosity may be fitted to an

Arrhenius equation of the form:

$$\log_{10}\eta = \log_{10}\eta_0 - V_a P / 2.303RT, \quad (2)$$

where *P* is the pressure (dyne/cm<sup>2</sup>), log<sub>10</sub>η<sub>0</sub> is the pre-exponential or frequency factor, *R* is the gas content and *V<sub>a</sub>* is the activation volume (cm<sup>3</sup>/mole) for viscous flow. The calculated activation volumes (Table 3) for AbF<sub>2</sub>O<sub>-1</sub> melt are 1.26 ± 0.19 and 1.14 ± 0.09 cm<sup>3</sup>/mole, at 1200° and 1400°C, respectively. The 0.001 kbar temperature dependence of the viscosity of AbF<sub>2</sub>O<sub>-1</sub> melt is Arrhenian [9]. Therefore, the temperature dependence of the viscosity of this melt at 7.5, 15 and 22.5 kbar has been calculated (Table 3) according to the following Arrhenius relationship:

$$\log_{10}\eta = \log_{10}\eta_0 + E_a / 2.303RT, \quad (3)$$

where *T* is the temperature (K) and *E<sub>a</sub>* (kcal/mole) is the activation energy of viscous flow. The activation energy of AbF<sub>2</sub>O<sub>-1</sub> melt decreases from 45.5 kcal/mole at 7.5 kbar to 33.8 kcal/mole at 22.5 kbar.

The AbH<sub>2</sub>O melt decreases in viscosity with

TABLE 3

Arrhenius parameters <sup>a</sup>

Composition	Temperature (°C)	<i>V<sub>a</sub></i> (cm <sup>3</sup> /mole)	Log <sub>10</sub> η <sub>0</sub>
	AbH <sub>2</sub> O	1400	0.45 ± 0.35
AbF <sub>2</sub> O <sub>-1</sub>	1400	1.14 ± 0.09	3.43 ± 0.04
	1200	1.26 ± 0.19	4.16 ± 0.10
Composition	Pressure (kbar)	<i>E<sub>a</sub></i> (kcal/mole)	Log <sub>10</sub> η <sub>0</sub>
	AbF <sub>2</sub> O <sub>-1</sub>	0.001	45.5
	7.5	35.2	-1.25
	15.0	33.8	-1.25
	22.5	33.8	-1.70

<sup>a</sup> Uncertainties quoted at 1σ.

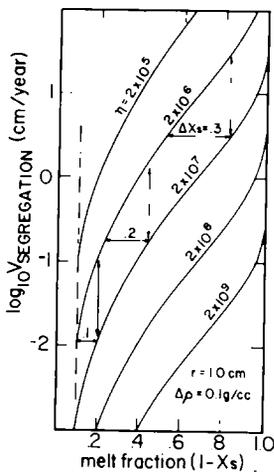


Fig. 4. The effects of melt viscosity ( $\eta$ ) and melt fraction ( $1 - X_s$ ) on the rate of crystal-melt segregation in lower crustal granitic melts.

increasing pressure from  $650 \pm 100$  P at 7.5 kbar to  $400 \pm 60$  P at 22.5 kbar (Table 3). At  $1400^\circ\text{C}$  the high-pressure (7.5–22.5 kbar) activation volume of the hydrous albite melt is  $0.45 \pm 0.35$   $\text{cm}^3/\text{mole}$ . The viscosity of this composition, calculated from the method of Shaw (562 P, [18]), is remarkably close to the observed high-pressure range. It is not clear, however, how well the low pressure (1–2 kbar) viscosity of albite + 2.79 wt.% water would agree with this calculated value. The viscosity of the  $\text{AbH}_2\text{O}$  melt is lower than the viscosity of the  $\text{AbF}_2\text{O}_{-1}$  melt at all pressures. The pressure dependence of viscosity of the  $\text{AbH}_2\text{O}$  melt is substantially less than that for the  $\text{AbF}_2\text{O}_{-1}$  melt.

The effects of  $\text{F}_2\text{O}_{-1}$  and  $\text{H}_2\text{O}$  on the viscosity of albite melt may be read from Fig. 3 by comparison of the data on albite melt at  $1400^\circ\text{C}$  with the results of this study at the same temperature. It is clear from Fig. 4 that  $\text{F}_2\text{O}_{-1}$  and  $\text{H}_2\text{O}$  both strongly decrease the viscosity of albite melt. This viscosity decrease is smaller at higher pressure. On an equimolar basis of total added  $\text{F}_2\text{O}_{-1}$  and  $\text{H}_2\text{O}$ , water has the larger effect on the viscosity of albite melt.

#### 4. Discussion

##### 4.1. Structural implications

It is generally accepted that albite melt has a three-dimensional network structure of intercon-

nected aluminate and silicate tetrahedra [12–14], with each aluminate tetrahedron stabilized by the presence of a charge-balancing sodium cation. Such a melt structure, where all oxygens form bridging bonds between pairs of tetrahedral cations, is said to be fully polymerized. The addition of any chemical components, except those that can form charge-balanced tetrahedra (e.g.,  $\text{KAlO}_2$ ,  $\text{NaAlO}_2$ ,  $\text{SiO}_2$ ) and maintain the three-dimensional structure, will result in a disruption of the three-dimensional network structure. Thus the addition of  $\text{Na}_2\text{O}$  to albite melt creates a depolymerized structure in which structural units containing nonbridging oxygens are coordinated by the excess sodium. This type of depolymerization results in a decrease in melt viscosity [4].

Clearly, both the substitution of fluorine for oxygen and the addition of water result in strong decreases in melt viscosity because neither fluorine nor water can be incorporated in the structure of albite melt without disruption of oxygen bridges. The negative pressure dependence of viscosity exhibited by  $\text{AbH}_2\text{O}$  and  $\text{AbF}_2\text{O}_{-1}$  contrasts with the positive pressure dependence of viscosity observed for (1) anhydrous depolymerized melts of diopside and sodium metasilicate composition [6], and (2) hydrous calcalkalic andesite [11]. This qualitative difference in pressure dependence may indicate that, despite their fluorine and water contents, the melts of this study remain more polymerized than the diopside, sodium metasilicate and hydrous andesite melts.

The solution of water in albite melt ruptures a number of (Si,Al)–O (Si,Al) bridges to produce Si–OH bonds [19–21]. Estimates of the yield of Si–OH bonds per mole of added water range from complete dissociation of added water [19,21] to approximately 66% dissociation at 2.79 wt.% added water [20]. In addition to solution of water by formation of Si–OH bonds [19] and as molecular water [20], Mysen et al. [21] have proposed, on the basis of spectroscopic studies, that non-bridging oxygens are formed by indirect depolymerization of the melt during the solution of water. Specifically, some of the water is associated with sodium as neutral complexes [19] that result in an excess of aluminum, which is expelled by the silicate network to form network-modifying aluminum co-

ordinated by non-bridging oxygens (NBO) [21].

The exchange of fluorine for oxygen in albite melt must also result in elimination of some oxygen-bridging bonds. Fluorine, like water, has two possible depolymerization mechanisms. Raman spectra of fluorine-bearing silica glass [22] corroborate previous suggestions [23,24] that fluorine in this melt forms Si-F bonds. In  $\text{AbF}_2\text{O}_1$  melt, however, it has been proposed [25] that fluorine is associated with sodium and aluminum in the form of charge-balanced complexes. This suggestion is in agreement with previous investigations of alkali aluminosilicate melts with some fluorine substituted for oxygen [26,27]. Specifically, in albite melt, fluorine has a greater affinity for sodium than aluminum and the resulting excess of aluminum is expelled from tetrahedral coordination. This aluminum is a network modifier coordinated by non-bridging oxygens [25].

In simple systems such as albite- $\text{Na}_2\text{O}$ ,  $\log \eta$  is a linear function of mole fraction  $\text{Na}_2\text{O}$  [4,28] and therefore, of  $\text{NBO}/T$ . Stolper [20, fig. 14] has implied that the decrease in  $\log \eta$  of a silicate melt with added water is proportional to the concentration of Si-OH bonds or non-bridging oxygens created in the melt. This concentration is, according to the solubility models of Burnham [19] and Stolper [20], linearly proportional to the value of  $\text{NBO}/T$  because these solubility models do not involve changes in the value of  $T$ . The ratio of the changes in  $\log$  viscosity of albite with added fluorine and added water is  $\Delta \log \eta_F / \Delta \log \eta_{\text{H}_2\text{O}} = 0.90 \pm 0.05$ ,  $0.84 \pm 0.05$  and  $0.97 \pm 0.05$  at 7.5, 15 and 22.5 kbar, respectively. Thus, if  $\log \eta$  is positively correlative with melt depolymerization ( $\text{NBO}/T$ ) in the system albite- $\text{F}_2\text{O}_1$ - $\text{H}_2\text{O}$ , then the decreases in  $\log$  viscosity lead to the inference that, at 1400°C, the addition of 2.79 wt.% water to albite melt results in a more depolymerized melt structure than the substitution of 5.8 wt.% fluorine for oxygen in albite melt.

#### 4.2. Geological implications

A large number of experimental studies are available to confirm the generation of water-rich (> 2 wt.%) granitic magmas within the earth's

crust at pressures of 5 to 15 kbar [29–31]. In most continental areas this pressure range corresponds to mid- to lower crustal depths of 15–45 km [32].

The results in Fig. 3 indicate that the effectiveness of fluorine and water in reducing melt viscosity extends, relatively undiminished, up to pressures relevant to the anatectic formation of granitic melts. Thus, dynamic processes operating during the formation and initial coalescence of granitic melts will be influenced by the relatively low viscosities of these melts.

In particular, the extent of restite-melt segregation during anatexis and magma coalescence is important in extracting the influence of source-region inhomogeneity on the generation of chemically complex batholiths. Incomplete crystal-melt segregation, the "restite hypothesis", has been used by some workers [33–35] to explain linear trace and major element variations within intrusive suites, but has been questioned recently [36].

The important parameter in determining melt distribution in a static, partially molten source region at very low degrees of partial melting is the surface energy. It is this energy that controls whether the melt will initially pool at grain triple points or infiltrate along grain edges to form a three-dimensionally interconnected melt reservoir [37,38]. At higher degrees of partial melting, or if a shear stress is applied to the static case described above, then the magma may behave dynamically with respect to the restite material. Depending on several variables, including melt fraction, crystal size, melt-crystal density contrasts and melt viscosity, restite crystals may or may not be entrapped within the coalescing melt fraction. At degrees of partial melting sufficiently large that crystal-melt segregation may be treated as crystal settling within a less dense viscous fluid, equation (4) describes the relationship between the velocity and the viscosity of crystal-melt segregation [39]:

$$V_s = 2a^2g\Delta\rho/9\eta M \quad (4)$$

This equation is a modified form of Stokes' law, where  $a$  is the radius of a (spherical) crystal,  $g$  is gravitational acceleration,  $\Delta\rho$  is the density contrast,  $\eta$  is melt viscosity and  $M$  is the term that accounts for the drag exerted by surrounding

crystals [39]. \* According to Arndt [39], the value of  $M$  may be approximated by the following function of solid fraction ( $X_s$ ):

$$M = (1 - X_s^{5/3}) / [1 - (9/4) X_s^{1/3} + (5/2) X_s - (9/4) X_s^{5/3} + X_s^2] \quad (5)$$

The value of  $M$  ranges over several orders of magnitude, and thus the volume fraction of restite strongly influences the rate of crystal-melt segregation. Fig. 4 illustrates the functional dependence of segregation velocity on viscosity ( $\eta$ ) and melt fraction ( $1 - X_s$ ). The efficiency of crystal-melt segregation in a coalescing magma batch depends not only on settling velocities but also on the scale and form of magma convection [3]. Therefore, in Fig. 4 it is the functional dependence of segregation velocity on melt viscosity and melt fraction, rather than the absolute magnitude of segregation velocity, that is emphasized. It is clear from Fig. 4 that a change in viscosity of an order of magnitude can shift the value of  $X_s$  corresponding to a given crystal-melt segregation velocity by a factor that is equivalent to 10, 20 or 30% of partial melting. Thus, if a critical value of crystal-melt separation velocity is necessary to achieve efficient melt segregation during partial melting [41], then the critical percentage of partial melt that can be extricated to form a distinct batch of melt will be strongly dependent on melt viscosity.

The viscosity-reducing effects of fluorine and water on silicate melts provide an explanation for certain geochemical features of water- and fluorine-rich granites and rhyolites. Firstly, there is little or no evidence for the control of major element chemistry by restite segregation in many fluorine- and water-rich granitic suites [36,42]. This behavior contrasts with geochemical trends commonly observed in water-undersaturated, fluorine-poor granitic suites. The absence of evidence

for restite separation in water- and fluorine-rich granitic suites is consistent with early, efficient separation of crystals and melt in a magma of relatively low viscosity. Secondly, fluorine-rich granites and rhyolites are commonly enriched in several incompatible elements including U, Be, Li, Rb, Th, Nb, Sn and W [42]. These enrichments are consistent with the derivation of fluorine-rich granites and rhyolites by unusually low degrees of partial melting of the lower crust.

## 5. Summary

The viscosities of  $\text{AbF}_2\text{O}_{-1}$  and  $\text{AbH}_2\text{O}$  melt decrease with increasing pressure from 7.5 to 22.5 kbar. The viscosity-reducing effects of fluorine and water on albite are not equivalent. At 1400°C, water is more effective on a molar equivalent basis ( $F = \text{OH}$ ) at concentrations of  $F/(F + \text{O}) = \text{OH}/(\text{OH} + \text{O}) = 0.1$ . The effects of water and fluorine on melt viscosity are consistent with the depolymerization of albite melt predicted from solution models for water and fluorine.

The results of this study have a direct bearing on the "restite hypothesis" of granitic magmas. It is not yet known whether fluorine and water have a significant effect on the surface energy of silicate melts, which is the major factor controlling the morphology of the partial melt fraction during low degrees of partial melting. The decrease in viscosity of albite melt with added fluorine and water, however, means that the segregation of a three-dimensionally interconnected partial melt phase from its restite will be greatly facilitated. Thus, fluorine and water may decrease the minimum degree of partial melt that can be effectively "tapped" from a lower crustal source region.

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\* It may be argued that if the melt fraction is very low, then the segregation of crystals from melt should be treated as the case of porous flow in a two-fluid medium [1,40]. The equations relating to such a treatment do not significantly change the conclusions regarding the dependence of segregation velocity on melt viscosity and porosity (i.e., melt fraction) (see [1]).

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